IN THE SPECIFICATION

Please substitute the following paragraph for the paragraph starting at page 10, line 1 and ending at line 16. A marked-up copy of this paragraph, showing the changes made thereto is attached.

In accordance with a preferred aspect of the invention, in the zoom lens, the following condition is satisfied:

$$vn(4F) - vp(4F) > 10$$

A1

where vn(4F) is, when the first lens subunit includes only one negative lens, an Abbe number of material of the negative lens included in the first lens subunit or, when the first lens subunit includes a plurality of negative lenses, a mean value of Abbe numbers of material of all the negative lenses included in the first lens subunit, and vp(4F) is, when the first lens subunit includes only one positive lens, an Abbe number of material of the positive lens included in the first lens subunit or, when the first lens subunit includes a plurality of positive lenses, a mean value of Abbe numbers of material of all the positive lenses included in the first lens subunit.

Please substitute the following paragraph for the paragraph starting at page 17, line 4 and ending at line 16. A marked-up copy of this paragraph, showing the changes made thereto is attached.

The amount of aberration $\Delta'Y$ of the entire lens system occurring when a lens unit p that is a part of the photographic lens is parallel-decentered by a distance E becomes the sum of the amount of aberration ΔY occurring before the parallel-decentering and the amount of decentering aberration $\Delta Y(E)$ produced by the parallel-decentering, as shown in the equation (a). Here, the amount of decentering aberration $\Delta Y(E)$ is represented, as shown in the equation (b),

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by using primary decentering coma (IIE), primary decentering astigmatism (IIIE), primary decentering curvature of field (PE), primary decentering distortion (VE1), primary decentering surplus distortion (VE2) and primary original point shift ΔE. (α'_k is the converted inclination angle of exit of outermost surface k in the entire lens system.)

Please substitute the following paragraph for the paragraph starting at page 23, line 13 and ending at line 22. A marked-up copy of this paragraph, showing the changes made thereto is attached.

A3

First, the conditions under which the image-stabilizing lens unit is made small in size and light in weight and is made optimum in terms of optical performance will be described in the following. The amount of decentering E4s of the image-stabilizing lens unit required for obtaining a predetermined amount of image-shake correction ΔY_p on an image plane is expressed by the following equation (m) on the basis of the equation (b) with R = 0, $\omega = 0$ and $\alpha_k' = 1$.

$$E4s = -\Delta Y_p / \{2(\Delta E)\} \quad \ldots (m)$$

Please substitute the following paragraph for the paragraph starting at page 23, line 23 and ending at page 24, line 4. A marked-up copy of this paragraph, showing the changes made thereto is attached.

A4

Since the primary original point shift (ΔE) is expressed by the equation (h), the amount of decentering E4s required for obtaining a necessary amount of image-shake correction ΔY_p is defined by using a converted inclination angle of incidence α and a converted inclination

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A4 end

angle of exit α' of an on-axial marginal ray on and from the image-stabilizing lens unit.

Accordingly, the zoom lens is made to satisfy the following condition (1):

$$\alpha' - \alpha < -0.45 \quad \ldots(1)$$

Please substitute the following paragraph for the paragraph starting at page 25, line 15 and ending at page 26, line 3. A marked-up copy of this paragraph, showing the changes made thereto is attached.

Accordingly, the zoom lens is made to satisfy the following condition (2):

$$\nu n(4F) - \nu p(4F) > 10 \quad \ldots(2)$$

where $\nu n(4F)$ is, when the image-stabilizing lens unit includes only one negative lens, an Abbe number of material of the negative lens included in the image-stabilizing lens unit or, when the image-stabilizing lens unit includes a plurality of negative lenses, a mean value of Abbe numbers of material of all the negative lenses included in the image-stabilizing lens unit, and $\nu p(4F)$ is, when the image-stabilizing lens unit includes only one positive lens, an Abbe number of material of the positive lens included in the image-stabilizing lens unit or, when the image-stabilizing lens unit includes a plurality of positive lenses, a mean value of Abbe numbers of material of all the positive lenses included in the image-stabilizing lens unit.

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Please substitute the following paragraph for the paragraph starting at page 28, line 21 and ending at page 29, line 16. A marked-up copy of this paragraph, showing the changes made thereto is attached.

Further, in the zoom lens according to embodiment of the invention, an optical system (4E) for shifting the range of variable magnification toward the telephoto side or the

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wide-angle side may be made to be located on the image side of the image-stabilizing lens unit by such a unit switching method as to detachably insert a lens unit, such as a built-in extender conversion optical system. In that instance, it is unnecessary to change the control of the image-stabilizing lens unit before and after the shift of the range of variable magnification. Fig. 27B is an optical conceptual diagram showing the zoom lens when the extender conversion optical system (focal-length conversion optical system) 4E is inserted in a position on the image side of the image-stabilizing lens unit. Since, as shown in Fig. 27B, the disposition of lens units on the object side of the image-stabilizing lens unit does not change before and after the shift of the focal length due to the insertion or detachment of the extender conversion optical system 4E, the amount of decentering E4s of the image-stabilizing lens unit required for obtaining a desired correction angle θ also does not change, so that it is unnecessary to change the control of the image-stabilizing lens unit.

Please substitute the following paragraph for the paragraph starting at page 30, line 25 and ending at page 31, line 12. A marked-up copy of this paragraph, showing the changes made thereto is attached.

The image-stabilizing lens unit is composed of one negative lens and one positive lens. When a converted inclination angle of incidence of a light flux on the image-stabilizing lens unit is denoted by α, a converted inclination angle of exit of a light flux from the image-stabilizing lens unit 4F denoted by α′, an Abbe number of material of the negative lens of the image-stabilizing lens unit is denoted by vn(4F), and an Abbe number of

material of the positive lens of the image-stabilizing lens unit is denoted by vp(4F), the above-mentioned conditions (1) and (2) are satisfied as shown by the following values:

$\alpha' - \alpha = -0.503$

$\nu n(4F) - \nu p(4F) = 22.7$

($\nu n(4F) = 46.6$,

$\nu p(4F) = 23.9$)

Please substitute the following paragraph for the paragraph starting at page 35, line 3 and ending at line 24. A marked-up copy of this paragraph, showing the changes made thereto is attached.

The fourth lens unit is composed of a lens subunit 4F of negative refractive power and a lens subunit 4R of positive refractive power. The whole lens subunit 4F serves as the image-stabilizing lens unit, having the function of moving in a direction perpendicular to the optical axis for the purpose of stabilizing an image. The image-stabilizing lens unit is composed of two negative lenses and one positive lens. When a converted inclination angle of incidence of a light flux on the image-stabilizing lens unit is denoted by α, a converted inclination angle of exit of a light flux from the image-stabilizing lens unit is denoted by α', a mean value of Abbe numbers of material of the negative lenses of the image-stabilizing lens unit is denoted by $\nu n(4F)$, and an Abbe number of material of the positive lens of the image-stabilizing lens unit is